

**Amendments to the specification:**

On page 1, line 3, please amend the heading as follows:

~~Prior Art~~ Background of the Invention

On page 1, please amend the first paragraph as follows:

In wiper blades of the present invention ~~type described in the preamble to claim 1~~, the support element should assure a predetermined distribution of the wiper blade pressing force – often also called pressure – applied by the wiper arm against the window, over the entire wiping zone that the wiper blade sweeps across. Through an appropriate curvature of the unstressed support element – i.e. when the wiper blade is not resting against the window – the ends of the wiper strip, which is placed completely against the window during the operation of the wiper blade, are loaded in the direction of the window by the support element, which is then under stress, even when the curvature radii of spherically curved vehicle windows change in every wiper blade position. The curvature of the wiper blade must therefore be slightly sharper than the sharpest curvature measured in the wiping zone of the window to be wiped. The support element thus replaces the costly support bracket design that has two spring strips disposed in the wiper strip, which is the kind used in conventional wiper blades (DE-OS 15 05 357).

On page 3, line 7, please amend the heading as follows:

~~Advantages~~ Summary of the Invention

Please amend the paragraph bridging pages 5-6 as follows:

The wiper blade according to the invention ~~, with the features of claim 10,~~ has the advantage that only one parameter has to be varied in order to adjust the outwardly decreasing contact force distribution. The curvature or the curvature progression along the support element can be preset in freely programmable bending machines. As a result, short trial runs can also be carried out to optimize the contact force distribution and therefore the curvature progression rapidly and without a great deal of expense. It is particularly advantageous if the coordinate that governs the curvature progression extends along the inertial element. This eliminates the need for complex reverse calculations in a Cartesian coordinate system in which each change in a position x requires a shifting of the subsequent "x values".

Please amend the paragraph bridging pages 6-7 as follows:

A wiper blade according to the invention ~~, with the features of claim 15,~~ excels in that without special adaptation, an excellent wiping result is achieved for average window types. The very simple steps taken result in the fact that the contact force distribution fulfills the requirements in most cases. The support points mentioned above are sufficiently precise to use as the basis for a curvature progression to be maintained.

On page 7, please amend the second paragraph as follows:

~~A wiper blade according to claim 15 is optimized through the steps taken in claim 16.~~ Even with complex window curvature progressions, the wiping quality can be increased by presetting the contact force distribution to particular support points. It is nevertheless possible to design the wiper blade without complex calculations. The curvature progression can be essentially predetermined and can be optimized by means of simple trials. An excellent wiping quality is assured as long as the prerequisites are met that the contact force distribution that prevails when the wiper blade is pressed against the window to be wiped is greater in a region approximately halfway between the center and the end of the wiper blade than it is at the end of the wiper blade.

On page 14, please amend the paragraph contained in lines 3-5 as follows:

For the most frequently occurring case of a rectangular profile 40, as shown in ~~Fig. 3~~ Figures 8 and 9, the moment of inertia is determined by:

On page 14, please amend the fourth paragraph as follows:

If the support element 12 is divided into two separate spring bars 42 and 44, as shown in ~~Fig. 4~~, Fig. 5, then in the above considerations in the first approximation, the width  $b$  can be assumed to be the sum of the individual widths

b1 and b2:  $b = b_1 + b_2$ . Hence simple relations between the width and thickness of a support element can also be deduced for systems of this kind.

On page 15, please amend the second paragraph as follows:

In order to achieve the quietest possible tilting over of the wiper lip 28 from its one drag position into its other drag position, the support element 12 that is used to distribute the contact force (arrow 24) is designed so that the contact force of the wiper strip 24, or rather the wiper lip 28, against the window surface 26 is greater in its middle section 36 (~~Fig. 11~~) than in at least one of the two end sections 38.

On page 18, please amend the paragraph contained in lines 6-21 as follows:

It has turned out that favorable wiping results can be achieved if the curvature  $K$  along the adaptive coordinate  $s$  is such that the contact force distribution, which prevails when the wiper blade is pressed against a flat window, is greater than in a region approximately halfway between the center and the end of the wiper blade than it is at the end of the wiper blade. Figs. 8 and 9 show this region ~~40~~ 50 for one side. The invention is based on the knowledge is of less significance than the relation between  $e$  that the progression of the contact force distribution  $p$  in the region ~~40~~ 50 to the contact force distribution  $p$  at the ends of the wiper blade. The overall length  $L$  of a wiper blade is plotted in Figs. 8 and 9, respectively, in which the connecting element 16

is disposed in the center of the wiper blade so that the wiper blade ends each  
occupy the value 0.5 L.